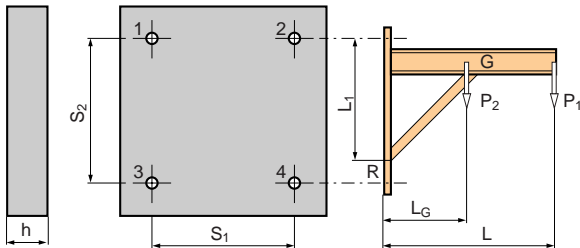


Examples

Example: SPIT TRIGA Z V12 anchor

Concrete : 25 Mpa – Non-cracked concrete

Thickness of base material : 200 mm



L = 1500 mm
 L_g = 750 mm
 S₁ = 165 mm
 S₂ = 220 mm
 No edge distance

P₁ = 6 kN
 P₂ = 100 kg

CALCULATION OF THE DESIGN ACTIONS PER ANCHOR :

$$N_{Sd} = 17,8 \text{ kN}$$

$$V_{Sd} = 1,75 \text{ kN}$$

We must verify $\beta_V^{1,5} + \beta_N^{1,5} \leq 1$

TENSILE LOAD :

→ $N_{Rd,p}$: failure mode not decisive

$$\rightarrow N_{Rd,c} = N_{Rd,c}^0 \times \Psi_{S1} \times \Psi_{S2}$$

$$N_{Rd,c}^0 = 24 \text{ kN}$$

$$S_1 = 165 \text{ mm} \rightarrow \Psi_{S1} = 0,84$$

$$S_2 = 220 \text{ mm} \rightarrow \Psi_{S2} = 0,96$$

$$N_{Rd,c} = 19,35 \text{ kN}$$

$$\rightarrow N_{Rd,s} = 44,9 \text{ kN}$$

$$\rightarrow N_{Rd} = \min(N_{Rd,p} ; N_{Rd,c} ; N_{Rd,s}) = 19,35 \text{ kN}$$

$$\rightarrow \beta_N = N_{Sd} / N_{Rd} \leq 1$$

$$\beta_N = 17,8 / 19,35 = 0,92$$

SHEAR LOAD :

$$\rightarrow V_{Rd,c} = V_{Rd,c}^0 \times \Psi_{S,c,N}$$

No edge distance → $c/c_{min} = 3,2$

$$S_1 = 165 \text{ mm} \rightarrow s/c_{min} = 2,0$$

$$\Psi_{S,c,N} = 3,46$$

$$V_{Rd,c} = 32,17 \text{ kN}$$

$$\rightarrow V_{Rd,s} = 58,2 \text{ kN}$$

$$\rightarrow V_{Rd} = \min(V_{Rd,c} ; V_{Rd,s}) = 32,17 \text{ kN}$$

$$\rightarrow \beta_V = V_{Sd} / V_{Rd} \leq 1$$

$$\beta_V = 1,75 / 32,17 = 0,05$$

COMBINED LOAD

$$\beta_V^{1,5} + \beta_N^{1,5} \leq 1$$

$$(0,92)^{1,5} + (0,05)^{1,5} = 0,89 \leq 1$$

The calculation is verified, so the anchor TRIGA Z V12 is suitable for this application.

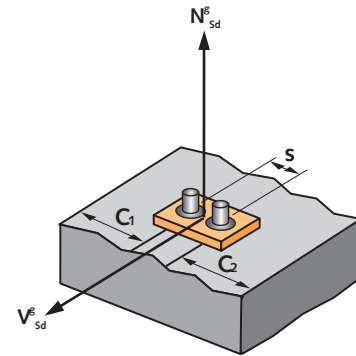
Examples

Example: SPIT FIX Z-A4 M10 anchor with minimum embedment

Cracked concrete – class C20/25
 Thickness of base material : 200 mm
 $S = 105 \text{ mm}$
 $C_1 = 100 \text{ mm}$
 $C_2 = 100 \text{ mm}$

DESIGN ACTIONS PER ANCHOR :

$N_{Sd} = 3,2 \text{ kN}$
 $V_{Sd} = 4,2 \text{ kN}$



We must verify $\beta_V^{1,5} + \beta_N^{1,5} \leq 1$

TENSILE LOAD :

$\rightarrow N_{Rd,p} = 4 \text{ kN}$

$\rightarrow N_{Rd,c} = N_{Rd,c}^0 \times \Psi_{S1} \times \Psi_{S2}$

$N_{Rd,c}^0 = 6,5 \text{ kN}$

$S = 100 \text{ mm} \rightarrow \Psi_S = 0,9$

$C1x = 100 \text{ mm} > (C_{cr,N} = 1,5 \cdot h_{ef}) \rightarrow \Psi_{C1X} = 1$

$C2x = 100 \text{ mm} > (C_{cr,N} = 1,5 \cdot h_{ef}) \rightarrow \Psi_{C2X} = 1$

$N_{Rd,c} = 5,85 \text{ kN}$

$\rightarrow N_{Rd,s} = 14,4 \text{ kN}$

$\rightarrow N_{Rd} = \min(N_{Rd,p}; N_{Rd,c}; N_{Rd,s}) = 4 \text{ kN}$

$\rightarrow \beta_N = N_{Sd} / N_{Rd} \leq 1$

$\beta_N = 3,2 / 4 = 0,8$

SHEAR LOAD :

$\rightarrow V_{Rd,c} = V_{Rd,c}^0 \times f_{\beta,V} \times \Psi_{S_c,N}$

Shear loading direction : angle $\beta = 90^\circ$ / edge concrete : $f_{\beta,V} = 2$

No edge distance in the shear direction $\rightarrow c/c_{min} = 3,2$

$S1 = 100 \text{ mm} \rightarrow s/c_{min} = 1,5$

$\Psi_{S_c,N} = 3,31$

$V_{Rd,c}^0 = 4,1 \text{ kN}$

$V_{Rd,c} = 27 \text{ kN}$

$\rightarrow V_{Rd,s} = 12 \text{ kN}$

$\rightarrow V_{Rd} = \min(V_{Rd,c}; V_{Rd,s}) = 12 \text{ kN}$

$\rightarrow \beta_V = V_{Sd} / V_{Rd} \leq 1$

$\beta_V = 4,2 / 12 = 0,35$

COMBINED LOAD

$\beta_V^{1,5} + \beta_N^{1,5} \leq 1$

$(0,8)^{1,5} + (0,35)^{1,5} = 0,92 \leq 1$

The calculation is verified, so the anchor FIX Z-A4 M10 (minimum anchorage) is suitable for this application.

Examples

Example: SPIT EPOMAX M16 anchor (with MAXIMA rod)

Non-cracked concrete – class C20/25

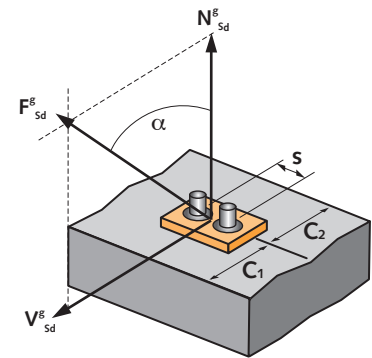
Thickness of base material : 350 mm

$S = 130$ mm

$C_1 = 170$ mm

$C_2 = 170$ mm

An oblique load $F_{Sd}^E = 28$ kN with $F_{Sd}^E = 55^\circ$ is applied in the middle of the base plate



$$N_{Sd}^E = F_{Sd}^E \times \cos(55^\circ) = 28 \times \cos(55^\circ) = 16 \text{ kN}$$

then per anchor $N_{Sd} = 16 / 2 = 8$ kN

$$V_{Sd}^E = F_{Sd}^E \times \sin(55^\circ) = 28 \times \sin(55^\circ) = 22,9 \text{ kN}$$

then per anchor $V_{Sd} = 22,9 / 2 = 11,45$ kN

TENSILE LOAD :

$$\rightarrow N_{Rd,p} = 23,1 \text{ kN}$$

$$\rightarrow N_{Rd,c} = N_{Rd,c}^0 \times \Psi_{S1} \times \Psi_{S2}$$

$$N_{Rd,c}^0 = 23,1 \text{ kN}$$

$$S = 130 \text{ mm} \rightarrow \Psi_S = 0,76$$

$$C_1 = C_2 = 170 \text{ mm} \rightarrow \Psi_C = 1$$

$$N_{Rd,c} = 17,55 \text{ kN}$$

$$\rightarrow N_{Rd,s} = 55,6 \text{ kN}$$

$$\rightarrow N_{Rd} = \min(N_{Rd,p}; N_{Rd,c}; N_{Rd,s}) = 17,55 \text{ kN}$$

$$\rightarrow \beta_N = N_{Sd} / N_{Rd} \leq 1$$

$$\beta_N = 8 / 17,55 = 0,45$$

SHEAR LOAD :

$$\rightarrow V_{Rd,c} = V_{Rd,c}^0 \times f_{\beta,V} \times \Psi_{S_c,N}$$

Shear loading direction : angle $\beta = 0^\circ$ / edge concrete : $f_{\beta,V} = 1$

$c_{min} = 65$ mm

$C_1 = 170$ mm - edge distance in the shear direction $\rightarrow c/c_{min} = 2,6$

$S = 130$ mm $\rightarrow s/c_{min} = 2,0$

$$\Psi_{S_c,N} = 2,63$$

$$V_{Rd,c}^0 = 5,7 \text{ kN}$$

$$V_{Rd,c} = 15 \text{ kN}$$

$$\rightarrow V_{Rd,s} = 32,9 \text{ kN}$$

$$\rightarrow V_{Rd} = \min(V_{Rd,c}; V_{Rd,s}) = 15 \text{ kN}$$

$$\rightarrow \beta_V = V_{Sd} / V_{Rd} \leq 1$$

$$\beta_V = 11,45 / 15 = 0,76$$

COMBINED LOAD

$$\beta_V^{1,5} + \beta_N^{1,5} \leq 1$$

$$(0,45)^{1,5} + (0,76)^{1,5} = 0,96 \leq 1$$

The calculation is verified, so the anchor EPOMAX M16 (with MAXIMA rod) is suitable for this application.